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(54) **HORIZONTAL TYPE SCROLL
COMPRESSOR**

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53/00; G01F 3/08; F01F 3/12
USPC 415/55.1, 54, 58
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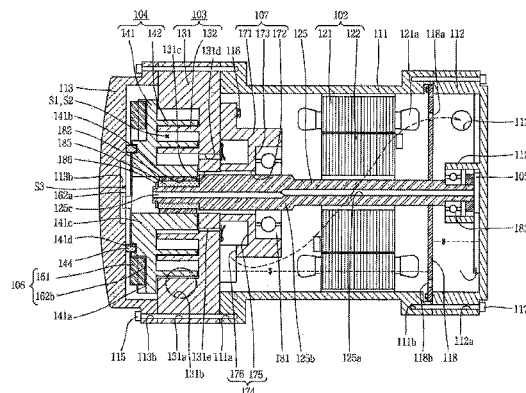
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(57)

ABSTRACT

A horizontal type scroll compressor includes a motor hous-
ing with a driving motor therein, a main scroll coupled to
one side of the motor housing and having a fixed wrap for
forming compression chambers, an orbiting scroll having an
orbiting wrap and coupled to a crankshaft inserted through
the main scroll, the orbiting scroll forming a first compres-
sion chamber and a second compression chamber on an
outer surface and an inner surface of the orbiting wrap while
performing an orbiting motion, and a front housing hermeti-
cally coupled to the main scroll. With the configuration, the
number of components and assembly parts may be reduced,
resulting in reduction of fabricating costs. Also, an inclina-
tion of the orbiting scroll can be prevented as the crankshaft
is inserted through the fixed wrap and the orbiting wrap.

15 Claims, 8 Drawing Sheets



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Fig. 1

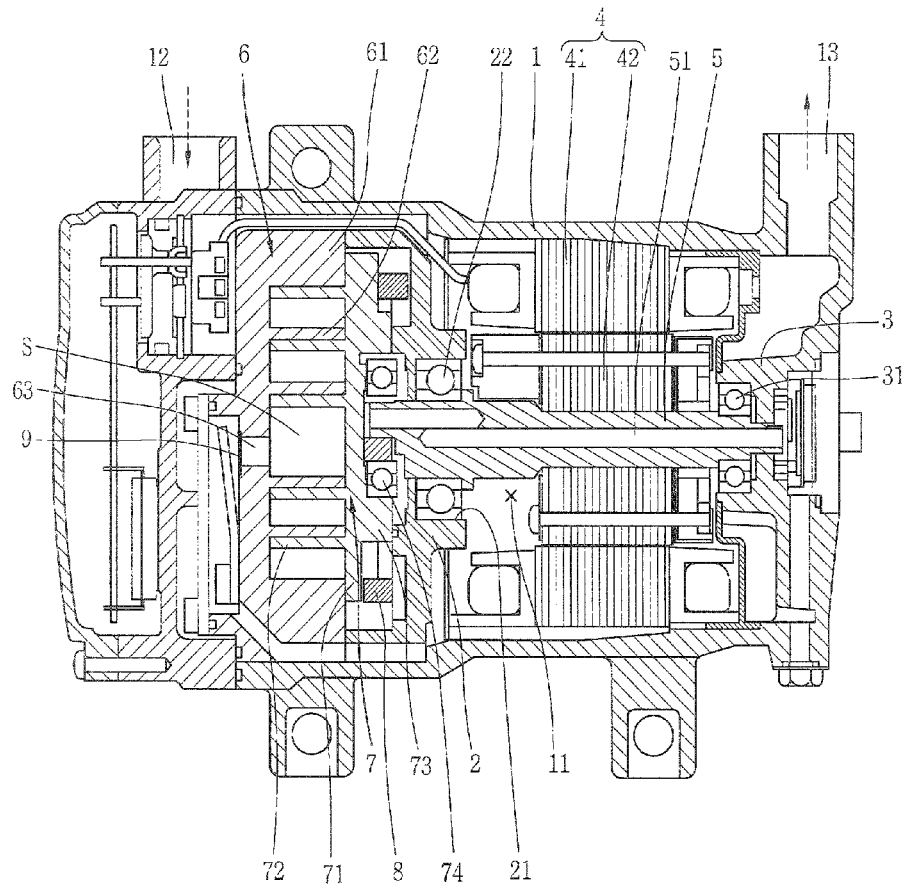
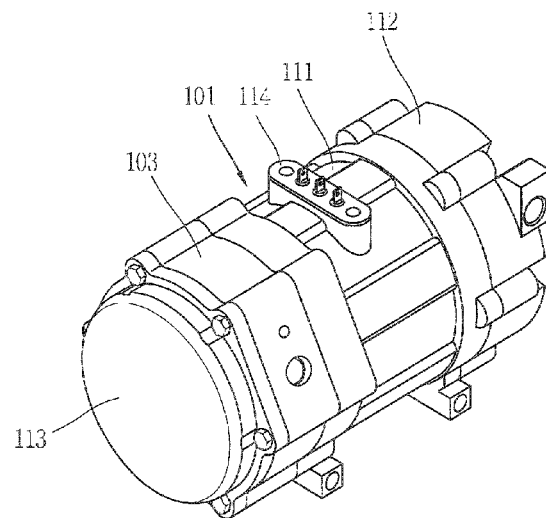


Fig. 2



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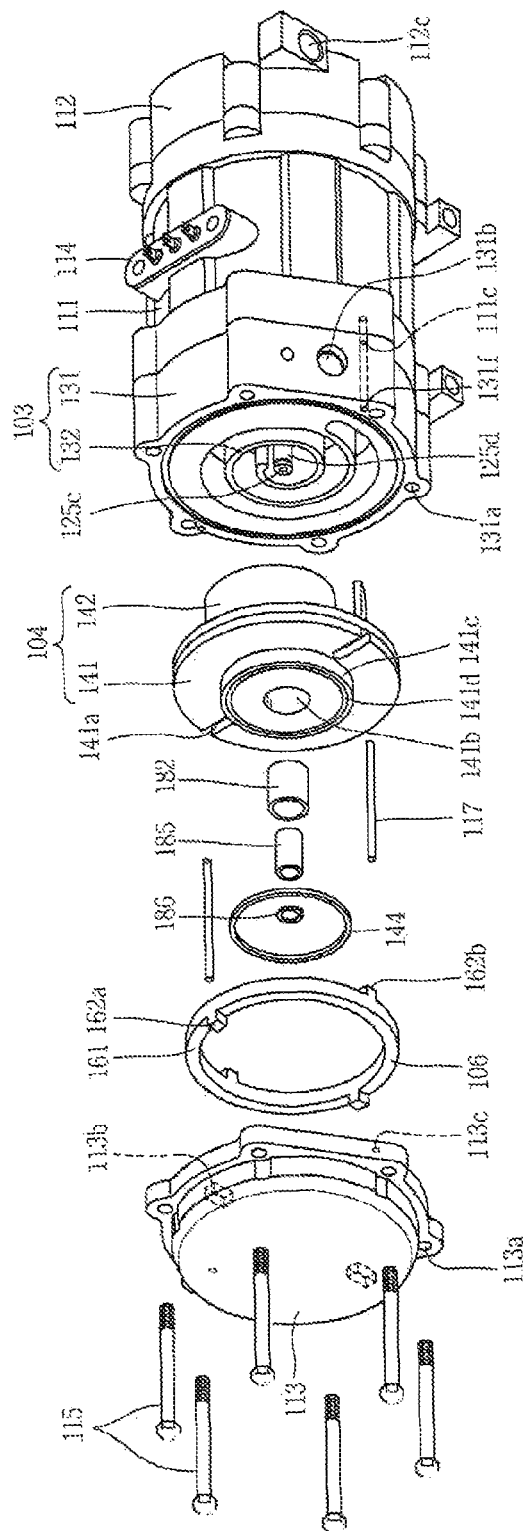


FIG. 4

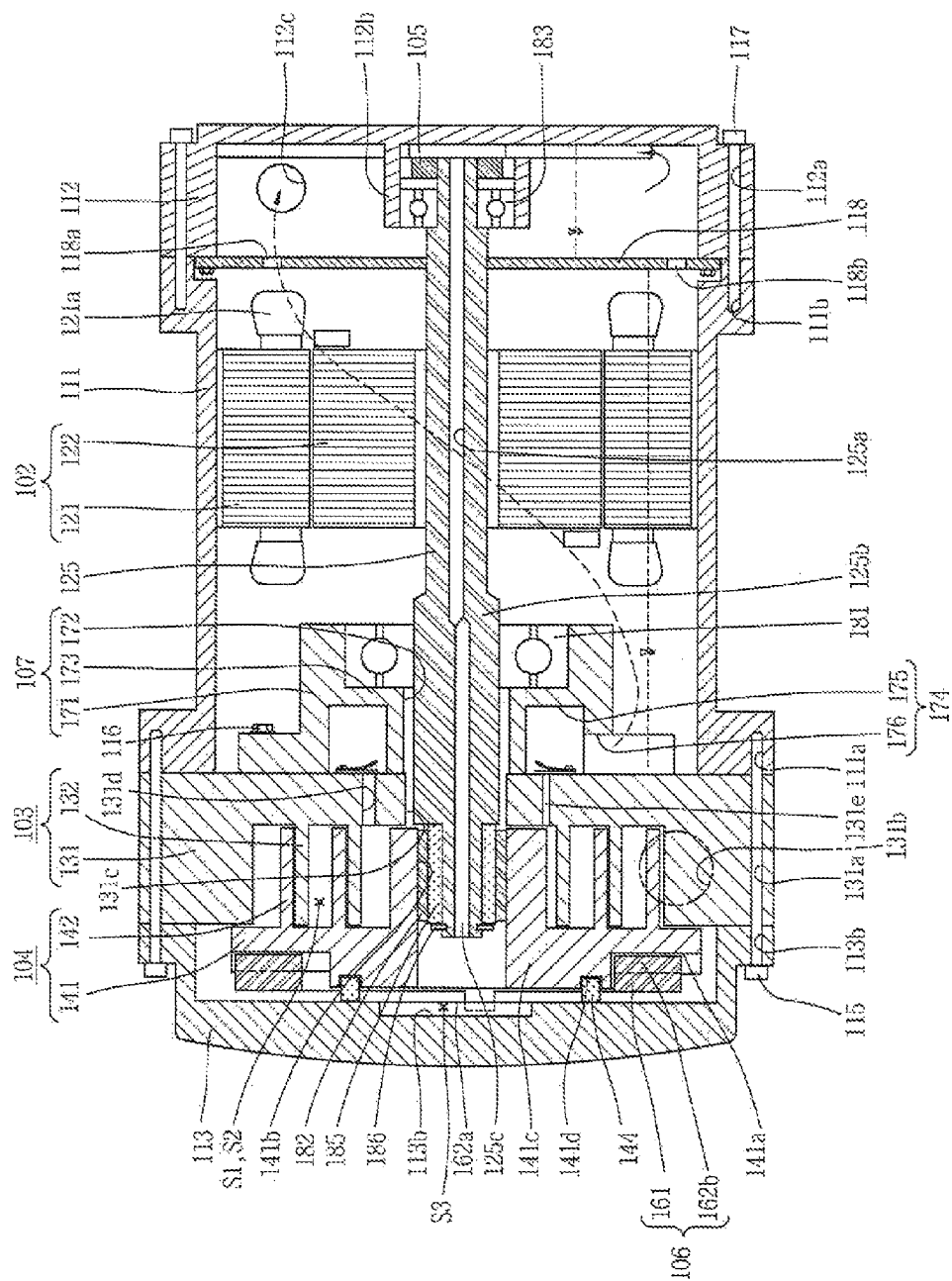


FIG. 6

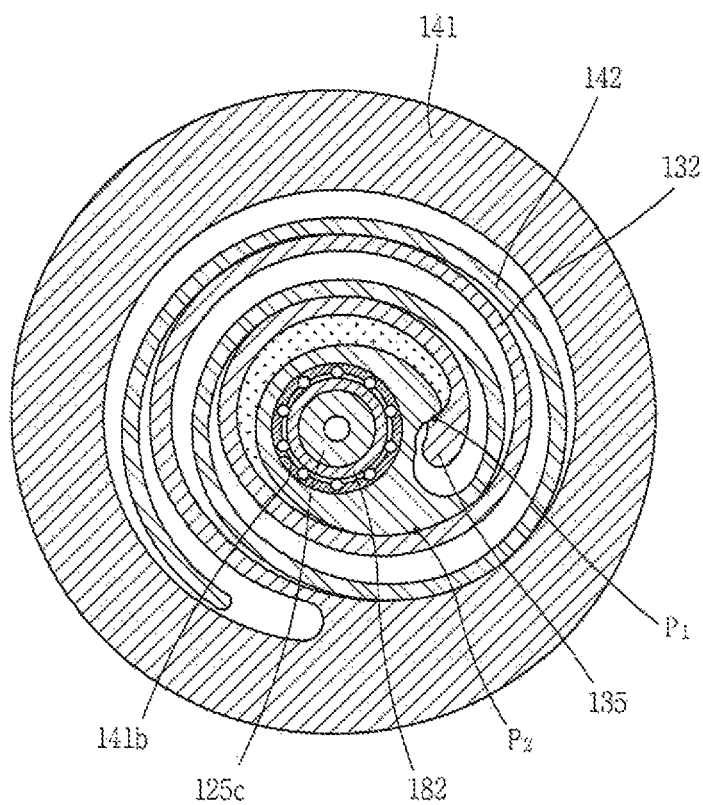


Fig. 7

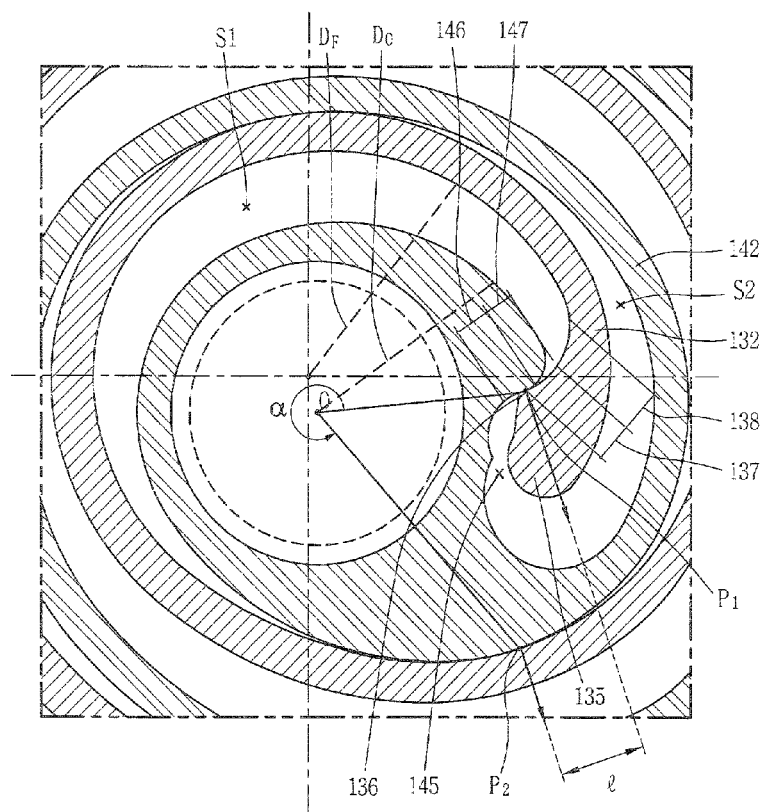


Fig. 8

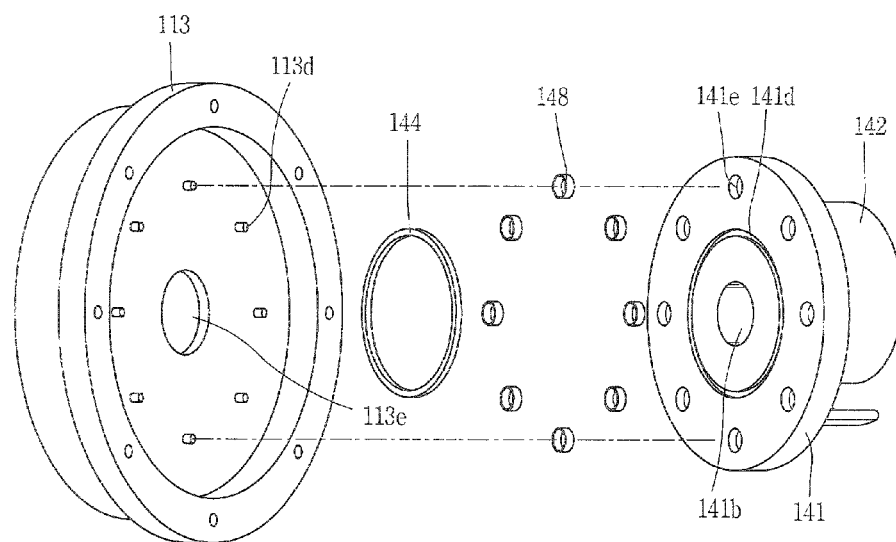


Fig. 9

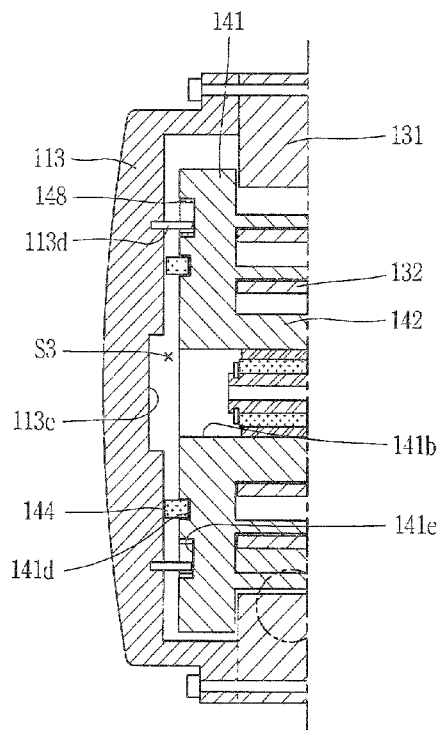


Fig. 10

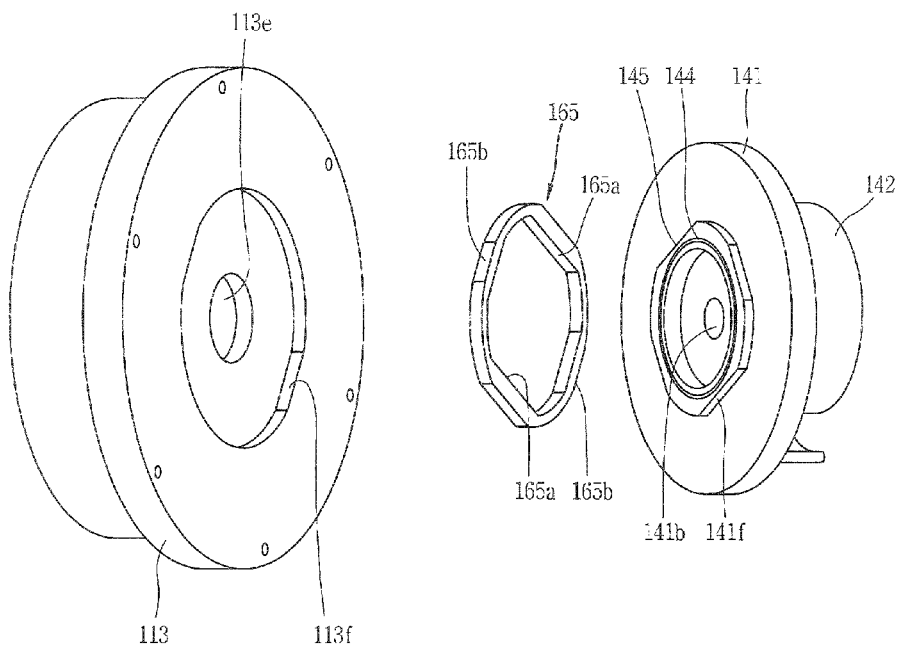
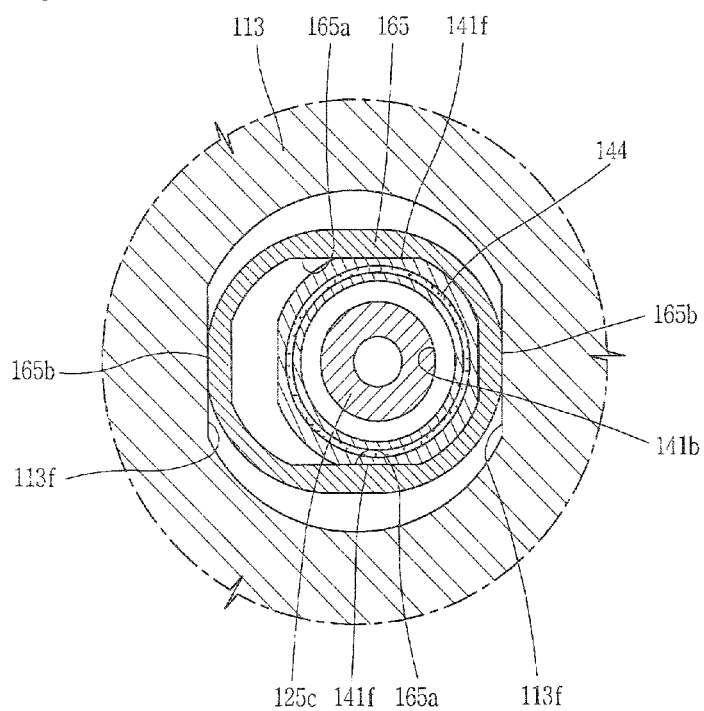


Fig. 11



1

HORIZONTAL TYPE SCROLL COMPRESSOR

CROSS-REFERENCE TO RELATED PATENT APPLICATIONS

This application is a U.S. National Stage Application under 35 U.S.C. §371 of PCT Application No. PCT/KR2013/001828, filed Mar. 7, 2013, which claims priority to Korean Patent Application No. 10-2012-0023532, filed Mar. 7, 2012, whose entire disclosures are hereby incorporated by reference.

TECHNICAL FIELD

The present disclosure relates to a horizontal type scroll compressor capable of being applied to vehicles.

BACKGROUND ART

In general, compressors are devices for compressing fluid such as refrigerant gas and the like, and may be classified into a rotary compressor, a reciprocal compressor, a scroll compressor and the like according to a method of compressing the fluid.

The scroll compressor is a high-efficiency and low-noise compressor which is widely applied to an air-conditioning field. The scroll compressor operates in the following manner. That is, while two scrolls respectively having a fixed wrap and an orbiting wrap orbit relatively, a plurality of compression chambers are formed as a pair between the fixed wrap and the orbiting wrap of each scroll. As their volumes of the compression chambers decrease while they continuously move toward their center, a refrigerant is continuously sucked, compressed and discharged.

Behaviors of the scroll compressor may depend on shapes of the fixed wrap and the orbiting wrap. Although they can have a random shape, the fixed wrap and the orbiting wrap typically have a shape of an involute curve which is easy to be processed. The involute curve refers to a curve corresponding to a track drawn by an end of a string, which is wrapped around a base circle having a random radius, when the string is unwound. Upon the use of the involute curve, wraps have a uniform thickness and accordingly a coefficient of volume change is constant. Therefore, in order to obtain a satisfactory compression ratio, the number of turns of the wrap has to increase. However, it also causes the compressor to increase in size.

FIG. 1 is a sectional view showing a structure of a horizontal type scroll compressor according to the related art.

As shown in FIG. 1, a scroll compressor according to the related art includes a main frame 2 and a sub frame 3 disposed within an inner space 11 of a casing 1 in a horizontal direction with a predetermined interval, a driving motor 4 installed between the main frame 2 and the sub frame 3 to generate a rotational force, and a crankshaft 5 formed in a center of a rotor 42 of the driving motor 4 and penetrating through the main frame 2 to be coupled to the orbiting scroll 7 so as to transfer the rotational force of the driving motor 4 thereto.

A fixed scroll 6 is fixed to a front of the main frame 2, and an orbiting scroll 7 is engaged with the fixed scroll 6 to form two compression chambers S as a pair which move continuously. An Oldham's ring 8 is installed between the orbiting scroll 7 and the main frame 2 such that the orbiting scroll 7 can orbit without rotation.

2

A shaft receiving hole 21 for supporting the crankshaft 5 in a radial direction is formed in the central portion of the main frame 2, and a main bearing 22 for supporting the crankshaft 5 in a radial direction is installed in the shaft receiving hole 21.

A fixed wrap 62 forming the pair of compression chambers S is formed in an involute shape on a rear surface of a fixed disk 61 of the fixed scroll 6. A suction port (not shown) is formed at a side surface of the fixed disk 61 to be directly connected to a suction pipe 13 such that a refrigerant can be sucked into the compression chambers S. A discharge port 63 is formed at a center of a front surface of the fixed disk 61 such that a refrigerant gas compressed in the compression chambers S can be discharged into the inner space 11 of the casing 1. A discharge valve 9 for opening or closing the discharge port 63 to prevent the refrigerant gas from flowing backwardly is disposed at a front surface of the fixed scroll 6.

An orbiting wrap 72 which forms two compression chambers S as a pair together with the fixed wrap 62 of the fixed scroll 6 is formed in an involute shape on a front surface of an orbiting disk 71 of the orbiting scroll 7. A boss portion 73 is formed at a center of a rear surface of the orbiting disk 61. The boss portion 73 is coupled to the crankshaft 5 to transfer the rotational force from the driving motor 4 to the crankshaft 5. A pin bearing 74 for support between the crankshaft 5 and the boss portion 73 in a radial direction is installed on an inner circumferential surface of the boss portion 73.

An unexplained reference numeral 12 denotes an inlet, 13 denotes an outlet, 31 denotes a sub bearing for supporting the crankshaft 4 in a radial direction, 41 denotes a stator of the driving motor 4, and 51 denotes an oil passage.

Hereinafter, description will be given of an operation of the related art scroll compressor.

That is, when power is applied to the driving motor 4, the crankshaft 5 rotates together with a rotor 42 of the driving motor 4. Accordingly, the orbiting scroll 7 orbits on an upper surface of the main frame 2 by the Oldham's ring 8 as far as an eccentric distance, and simultaneously, two, namely, a pair of compression chambers S are continuously formed between the fixed wrap 62 and the orbiting wrap 72. As the compression chambers move, with their volumes decreased, toward their center in response to a continuous orbiting motion of the orbiting scroll 7, a refrigerant gas is continuously, sucked, compressed and discharged.

DISCLOSURE OF INVENTION

Technical Problem

However, in the related art horizontal type scroll compressor, the main frame 2 and the fixed scroll 6 are separately installed within the casing 1, which causes an increase in the number of components. Also, the main frame 2 and the fixed scroll 6 have to be assembled to the casing 1, respectively, which increases the number of assembly parts, resulting in an increase in fabricating costs of the compressor.

Further, as the crankshaft 5 is coupled to the rear surface of the orbiting scroll 7, an application point to which a repulsive force of a refrigerant is applied is spaced apart in a vertical direction from an application point to which a reaction force for offsetting the repulsive force is applied during compression. Accordingly, the orbiting scroll 7 is inclined during operation, increasing vibration or noise. Especially, for the horizontal type scroll compressor, the

3

orbiting scroll 7 is further inclined by its own weight, which may be likely to further increase the vibration or noise of the compressor.

Solution to Problem

Therefore, to obviate those problems, an aspect of the detailed description is to provide a horizontal type scroll compressor, capable of reducing fabricating costs by reduction of the number of components and the number of assembly parts.

Another aspect of the detailed description is to provide a horizontal type scroll compressor, capable of overcoming a problem of an inclination of an orbiting scroll, in a manner of controlling an application point of a repulsive force of a refrigerant and an application point of the corresponding reaction force to be applied onto the same portion.

To achieve these and other advantages and in accordance with the purpose of the present invention, as embodied and broadly described herein, there is provided a horizontal type scroll compressor including a motor housing having an inner space for installation of a driving motor therein, a main scroll coupled to one side of the motor housing to seal the inner space of the motor housing, and having a fixed wrap for forming compression chambers, an orbiting scroll having an orbiting wrap engaged with the fixed wrap of the main scroll and coupled to a crankshaft inserted through the main scroll, the orbiting scroll forming a first compression chamber and a second compression chamber on an outer surface and an inner surface of the orbiting wrap while performing an orbiting motion, and a front housing hermetically coupled to the main scroll, the front housing accommodating the orbiting scroll.

In accordance with another exemplary embodiment of the detailed description, there is provided a horizontal type scroll compressor including a casing, a driving motor installed within an inner space of the casing and having a rotor, a crankshaft coupled to the rotor, a main scroll coupled to the casing, the main scroll having a fixed wrap, and an orbiting scroll having an orbiting wrap engaged with the fixed wrap of the main scroll and coupled to a crankshaft inserted through the main scroll, the orbiting scroll forming a first compression chamber and a second compression chamber on an outer surface and an inner surface of the orbiting wrap while performing an orbiting motion, wherein a shaft coupling portion to which the crankshaft is inserted may be formed through the orbiting scroll.

Here, a plurality of pin members may be disposed on one of a rear surface of the orbiting scroll and the casing, and a plurality of pin recesses may be formed on the other one. The plurality of pin members may be inserted into the plurality of pin recesses to allow for orbiting of the orbiting scroll.

A ring member may be disposed between the rear surface of the orbiting scroll and the casing, the ring member preventing rotation of the orbiting scroll. An inner circumferential sliding surface and an outer circumferential sliding surface may be perpendicularly formed on an inner circumferential surface and an outer circumferential surface of the ring member, respectively. The sliding surfaces may slidably contact guide surfaces, respectively, in a radial direction. The guide surfaces may be disposed on the casing and the orbiting scroll, respectively.

The first compression chamber may be formed between two contact points P1 and P2 generated as an inner surface of the fixed wrap and an outer surface of the orbiting wrap contact each other. The crankshaft may include an eccentric

4

pin coupled to a shaft coupling portion of the orbiting scroll. Here, α may be 360° ($\alpha < 360^\circ$ at least before the beginning of discharging when it is assumed that α is a larger angle of angles formed by two lines connecting a center O of the eccentric pin of the crankshaft and the two contact points P1 and P2, respectively).

Advantageous Effects of Invention

In accordance with the detailed description, in the horizontal type scroll compressor, the main scroll forming the fixed scroll may be located between the motor housing and the front housing to be fixed to both of them. This may allow the fixed scroll to be installed without a separate frame, resulting in reduction of the number of components. In addition, the number of assembly parts may be reduced by coupling the motor housing, the main scroll and the front housing all together by use of long coupling bolts, reducing fabricating costs accordingly.

Also, the crankshaft may be inserted through the fixed wrap of the main scroll and the orbiting wrap of the orbiting scroll. This may allow an application point of a repulsive force of a refrigerant and an application point of a corresponding reaction point to be applied to the same portion, thereby preventing the orbiting scroll from being inclined. With forming the protrusion and the concave portion at the discharge side of the fixed wrap and the orbiting wrap, a compression ratio of a first compression chamber may be improved and a thickness of an inner end portion of the fixed wrap may increase. This may result in improvement of a wrap strength and a leakage-preventing function.

BRIEF DESCRIPTION OF DRAWINGS

FIG. 1 is a longitudinal sectional view showing one exemplary embodiment of a scroll compressor according to the related art;

FIG. 2 is a perspective view showing one exemplary embodiment of a horizontal type scroll compressor in accordance with the present disclosure;

FIG. 3 is a disassembled perspective view of the horizontal type scroll compressor of FIG. 2;

FIG. 4 is an assembled longitudinal sectional view of the horizontal type scroll compressor of FIG. 2;

FIG. 5 is a longitudinal sectional view showing a compression part in the horizontal type scroll compressor of FIG. 4;

FIG. 6 is a horizontal sectional view showing one exemplary embodiment of a fixed wrap and an orbiting wrap defining the compression part in the horizontal type scroll compressor of FIG. 4;

FIG. 7 is an enlarged horizontal sectional view showing surroundings of final compression chambers formed by the fixed wrap and the orbiting wrap of FIG. 6;

FIGS. 8 and 9 are a disassembled perspective view and an assembled sectional view, respectively, showing another exemplary embodiment of an anti-rotation member in the horizontal type scroll compressor of FIG. 3; and

FIGS. 10 and 11 are a disassembled perspective view and an assembled sectional view, respectively, showing another exemplary embodiment of an anti-rotation member in the horizontal type scroll compressor of FIG. 3.

BEST MODE FOR CARRYING OUT THE INVENTION

Embodiments of the present invention will be described below in detail with reference to the accompanying draw-

5

ings where those components are rendered the same reference number that are the same or are in correspondence, regardless of the figure number, and redundant explanations are omitted. In describing the present invention, if a detailed explanation for a related known function or construction is considered to unnecessarily divert the gist of the present invention, such explanation has been omitted but would be understood by those skilled in the art. The accompanying drawings are used to help easily understood the technical idea of the present invention and it should be understood that the idea of the present invention is not limited by the accompanying drawings. The idea of the present invention should be construed to extend to any alterations, equivalents and substitutes besides the accompanying drawings.

FIG. 2 is a perspective view showing one exemplary embodiment of a horizontal type scroll compressor in accordance with the present disclosure, FIG. 3 is a disassembled perspective view of the horizontal type scroll compressor of FIG. 2, FIG. 4 is an assembled longitudinal sectional view of the horizontal type scroll compressor of FIG. 2, and FIG. 5 is a longitudinal sectional view showing a compression part in the horizontal type scroll compressor of FIG. 4.

As shown in those drawings, a horizontal type scroll compressor according to the present disclosure may include a driving motor **102** installed within a casing **101** to generate a rotational force, a main scroll **103** coupled to one side (hereinafter, referred to as a front side) of the casing **101** to form a compression part as well as covering the casing **101**, an orbiting scroll **104** coupled to a front side of the main scroll **103** to form the compression part together with the main scroll **103**, and an oil pump **105** installed at another side (hereinafter, referred to as a rear side) of the driving motor **102** to supply oil stored within the casing **101** into the compression part.

The casing **101** may include a motor housing **111** having both ends open and the driving motor **102** installed therein, a pump housing **112** for covering the rear open end of the motor housing **111** and mounting the oil pump therein, and a front housing **113** coupled to the main scroll **103**, which covers the front open end of the motor housing **111**, so as to accommodate the orbiting scroll **104** therein.

Here, the main scroll **103** may be installed between the motor housing **111** and the front housing **113** to define a part of the casing **101**. The front housing **113** may be coupled to the motor housing **111**, with being spaced apart from the motor housing **111** by a thickness of a frame portion **131** of the main scroll **103**, by use of coupling bolts **115**, which are long enough to be inserted through the frame portion **131**, which will be explained later.

The motor housing **111**, the main scroll **103** and the front housing **113** may be coupled in an aligned state by using a plurality of reference pins **117**, which are inserted through reference recess **111c** formed on the motor housing **111** and reference recesses **113c** formed on the front housing **113**, and reference holes **131f** formed on the main scroll **103** in a sequential manner.

The motor housing **111** may have a cylindrical shape, and its both open ends may be provided with coupling bores **111a** and **111b** for coupling of bolts. A terminal part **114** electrically connected to a coil **121a** of the driving motor **102** may be formed at one side on an outer circumferential surface of the motor housing **111**.

The driving motor **102** may include a stator **121** fixed to the motor housing **111** in a manner of shrink fitting or bolt coupling, and a rotor **122** rotatably coupled into the stator **121**. The stator **121** may be wound by a coil **121a**, and a

6

crankshaft **125** for transferring the rotational force to the orbiting scroll **104** may be coupled into a center of the rotor **122**.

An oil passage **125a** may be extendedly formed in a central portion of the crankshaft **125** in a lengthwise direction of the crankshaft **125**. An oil pump **105** may be installed at one end (e.g., a rear end) of the crankshaft **125** for supplying oil stored in the pumping housing **112** to another end (e.g., a front end) of the crankshaft **125**. The oil pump **105** may be implemented as a positive displacement pump having a trochoid gear.

A diameter-extending portion **125b** which is inserted into a main bearing **181** disposed in a bearing guide **107** to be explained later may be formed at a front end of the crankshaft **125**. An eccentric pin **125c** inserted into a shaft coupling portion **141b** of the orbiting scroll **104** to be explained later may be formed at an end portion of the diameter-extending portion **125b**. A bush **185** to be explained later may be coupled to the shaft coupling portion **141b** and a pin bearing **182** for supporting the eccentric pin **125c** may be coupled into the bush **185**. The pin bearing **182** may appropriately be implemented as a needle bearing having a characteristic that its load bearing capacity is great as compared with its diameter. The eccentric pin **125c** of the crankshaft **125** may be inserted into the pin bearing **182** implemented as the needle bearing to be supported in a radial direction.

The pump housing **112** may be formed in a shape of a cap whose front end is open. A coupling hole **112a** which aligns with the rear coupling bore **111b** of the motor housing **111** may be formed on the open end of the pump housing **112**.

A bearing support portion **112b** in which a sub bearing **183** for supporting the crankshaft **125** is installed may be formed in a central portion of the pump housing **112**, and the oil pump **105** may be installed on the other side of the bearing support portion **112b**.

An outlet **112c** for guiding a refrigerant discharged from the compression part to be introduced into a refrigerating cycle may be formed at one side of the pump housing **112**. A discharge pipe (not shown) may be connected to the outlet **112c**.

The front casing **113** may be formed in a shape of a cap whose rear end is open, and through holes **113a** may be formed through the open end of the front housing **113** to align with coupling holes **131a** of the main scroll **103** to be explained later.

First key recesses **113b** into which first keys **162a** of an Oldham's ring **106** to be explained later are slidably coupled may be recessed into a front surface at an inner side of the front housing **113**. The first key recesses **113b** may be formed long in a radial direction with an interval of 180°.

The main scroll **103** may include a frame portion **131** formed in a shape of plate, coupled to the front open end of the motor housing **111** and forming a fixed plate of the main scroll **103**, and a fixed side wrap portion **132** formed at a front of the frame portion **131** and engaged with an orbiting wrap **142** of the orbiting scroll **104** to be explained later to form a first compression chamber S1 and a second compression chamber S2. The fixed side wrap portion **132** defines a fixed wrap. Hereinafter, it will thusly be briefly referred to as a fixed wrap.

The frame portion **131** may be formed in a shape of a plate having a predetermined thickness, and include coupling holes **131a** formed on an edge thereof to align with the front coupling bore **111a** of the motor housing **111** and the coupling holes **113a** of the front housing **113**, such that coupling bolts **115** are coupled all thereinto.

An inlet **131b** may be formed on a side surface of the frame portion **131**, and a suction pipe (not shown) may be connected to the inlet **131b**.

A shaft hole **131c** through which the front end of the crankshaft **125** is inserted may be formed in a central portion of the frame portion **131**. A discharge port **131d** may be formed adjacent to the shaft hole **131c** such that a refrigerant compressed in the compression chambers S1 and S2 is discharged toward the motor housing **111**. The discharge port **131d** may also be formed out of a range of an outer diameter of a main bearing **181**, which will be explained later, to prevent it from overlapping the main bearing **181**. However, in this structure, a great dead volume may be generated in a central portion of a scroll. Therefore, the discharge port **131d** may preferably be formed adjacent to the shaft hole **131c** if possible. Bypass ports **131e** for bypassing in advance a part of a refrigerant compressed in the compression chambers S1 and S2 may be formed adjacent to the discharge port **131d**.

A bearing guide **107** for supporting the main bearing **181** may be coupled to a rear side surface of the frame portion **131** by use of bolts **116**.

The bearing guide **107**, as shown in FIG. 4, may include a guide body **171** formed in a cylindrical shape, a shaft receiving portion **172** formed through a middle of an inner circumferential surface of the guide body **171** and having a through hole for insertion of the crankshaft **125** therethrough. The guide body **171** may have one end bent to be coupled to the rear side surface of the main scroll **103** by use of the bolt **116**. The guide body **171** may have an area large enough for a discharge guide portion **174**, which will be explained later, to accommodate the discharge port **131d** and the bypass ports **131e** therein.

A bearing mounting portion **173** in which the main bearing **181** implemented as a ball bearing is inserted may be formed on one side surface of the shaft receiving portion **172**. The discharge guide portion **174** for guiding a refrigerant discharged from the compression chambers toward the motor housing **111** may be formed at another side surface of the shaft receiving portion **172**.

The bearing mounting portion **173** may be formed in a circular shape to have approximately the same inner diameter as an outer diameter of the main bearing **181**.

The discharge guide portion **174** may include a first guide passage **175** corresponding to an annular space defined by the guide body **171**, the shaft receiving portion **172** and a rear side surface of the main scroll **103**, and accommodating the discharge port **131d** and the bypass ports **131e** therein, and a second guide passage **176** formed by opening an outer circumferential surface of the first guide passage **175** such that a refrigerant introduced into the first guide passage **175** is discharged toward the motor housing **111**. The second guide passage **176** may be formed in plurality which are arranged along the outer circumferential surface of the first guide passage **175** with a predetermined interval.

In the meantime, the orbiting scroll **104** may include an orbiting plate **141** formed in a shape of plate to define a bearing surface together with the frame portion **131** of the main scroll **103**, and an orbiting side wrap portion **142** formed on a rear side of the orbiting plate **141** and engaged with the fixed wrap **132**. Here, the orbiting side wrap portion **142** may form an orbiting wrap. Therefore, the orbiting side wrap portion **142** may be briefly referred to as an orbiting wrap, hereinafter.

Second key recesses **141a** which are long in a radial direction to allow second keys **162b** of the Oldham's ring **160** to be slidably inserted may be recessed into a front

surface of the orbiting plate **141**. The second key recesses **141a** may be formed with an interval of 180° and have approximately 90° phase difference from the first key recesses **113b** of the front housing **113**.

The shaft coupling portion **141b** in which the eccentric pin **125c** of the crankshaft **125** is inserted may be formed through the center of the orbiting plate **141**. The bush **185** may be inserted into the shaft receiving portion **141b**. The bush **185** may be undetachably fixed to the shaft coupling portion **141b** by a bush fixing member, such as a snap ring **186**, which is fixedly inserted into a fixing groove **125d** formed on the eccentric pin **125c**.

A pin bearing **182** in which the eccentric pin **125c** of the crankshaft **125** is inserted may be coupled to the bush **185**. The pin bearing **182** may be implemented as a needle bearing as aforementioned.

Meanwhile, the fixed wrap **132** and the orbiting wrap **142** may be formed in a shape of involute curve. Upon the use of the involute curve, wraps have a uniform thickness and accordingly a coefficient of volume change is constant. Therefore, in order to obtain a satisfactory compression ratio, the number of turns of the wrap has to increase. However, it also causes the compressor to increase in size. Therefore, according to this exemplary embodiment, as shown in FIGS. 6 and 7, when it is assumed that a compression chamber, which is formed between two contact points P1 and P2 generated as an inner surface of the fixed wrap **132** comes in contact with an outer surface of the orbiting wrap **142**, is referred to as the first compression chamber S1, the first compression chamber S1 may be formed such that an angle defined by two lines which connect a center O of the eccentric pin **125c** of the crankshaft **125** to the respective two contact points P1 and P2 is smaller than 360 and a distance **1** between normal vectors at each contact point P1 and P2 is greater than 0. Accordingly, the first compression chamber S1 just before discharging may have a smaller volume, as compared with having the fixed wrap and the orbiting wrap in the shape of the involute curve. This may result in an increase in a compression ratio. In addition, the fixed wrap **132** and the orbiting wrap **142** may have a shape formed by connecting a plurality of circular arcs having different diameters and start points from one another, and the outermost curve may have an approximately oval shape with a major axis and a minor axis.

A protrusion **135** may be formed adjacent to an inner end portion of the fixed wrap **132**. The protrusion **135** may protrude toward the shaft coupling portion **141b** of the orbiting scroll **104**. A contact portion **136** may further protrude from the protrusion **135**. That is, the inner end portion of the fixed wrap **132** may be formed to be thicker than the other portions in thickness. This may improve a wrap strength of the inner end portion which is affected by the greatest compression force of the fixed wrap **132**, resulting in enhancement of durability.

As shown in FIG. 7, the thickness of the fixed wrap **132** may gradually decrease, starting from the inner contact point P1, which forms the first compression chamber S1 at the beginning of discharging, of the two contact points P1 and P2. In detail, a first decreasing portion **137** adjacent to the contact point P1 and a second decreasing portion **138** connected to the first decreasing portion **137** may be formed. A thickness decrease rate in the first decreasing portion **137** may be greater than that in the second decreasing portion **138**. After the second decreasing portion **138**, the fixed wrap **132** may continuously increase in thickness for a predetermined section.

A concave portion **145** which is engaged with the protrusion **135** may be formed at the shaft coupling portion **141b** of the orbiting scroll **140**. One side wall of the concave portion **145** may form one contact point of the first compression chamber S1 by contacting the contact portion **136** of the protrusion **135**.

The one side wall of the concave portion **145** may include a first increasing portion **146** whose thickness relatively drastically increases, and a second increasing portion **147** connected to the first increasing portion **146** and having a thickness increasing at a relatively low ratio. They correspond to the first decreasing portion **137** and the second decreasing portion **138** of the fixed wrap **132**. The first increasing portion, the first decreasing portion, the second increasing portion and the second decreasing portion may be obtained as a result of bending an envelope toward the shaft coupling portion **141b**. Accordingly, the inner contact point P1 forming the first compression chamber S1 may be located at the first increasing portion **146** and the second increasing portion **147** and also a length of the first compression chamber S1 just before discharging may be shortened. This may result in improvement of a compression ratio.

Another side wall of the concave portion **145** may have a shape of arc. A diameter of the arc may be decided by a wrap thickness of the end portion of the fixed wrap **132** and an orbiting radius of the orbiting wrap **142**. When the end portion of the fixed wrap **132** increases in thickness, the diameter of the arc may increase. The thickness of the orbiting wrap **142** near the arc may thusly increase so as to ensure durability. Also, a compression path may extend so as to increase a compression ratio of the second compression chamber S2.

Here, a central portion of the concave portion **145** may form a part of the second compression chamber S2. The second compression chamber S2 may contact the arcuate wall of the concave portion **145**. When the crankshaft **125** rotates a little bit more, one end of the second compression chamber S2 may pass through the central portion of the concave portion **145**.

Meanwhile, an Oldham's ring **106** as an anti-rotation member for guiding the orbiting scroll **104** to perform an orbiting motion may be installed between a front surface of the orbiting scroll **104** and a corresponding inner rear surface of the front housing **113**.

The Oldham's ring **106**, as shown in FIGS. 3 and 4, may include a ring portion **161** having an annular form, and first keys **162a** and second keys **162b** formed on front surface and rear surface of the ring portion **161**, respectively. The first keys **162a** may be formed with an interval of 180°, similar to the first key recesses **113b**. The second keys **162b** may also be formed with the interval of 180° similar to the first keys **162a**. The first key recesses **113b** and the second key recesses **141a** may be formed in a circumferential direction by an interval of 90° in an alternating manner.

In the meantime, a sealing member **144** for forming a back pressure chamber at the front of the orbiting scroll **104** may be disposed on the front surface of the orbiting scroll **104**. To this end, a sealing protrusion **141c** may be formed on a circumference of the shaft coupling portion **141b** of the orbiting scroll **104**, and a sealing recess **141d** in which the sealing member **144** is inserted may be formed on the sealing protrusion **141c**. Accordingly, a back pressure chamber S3 in a high pressure atmosphere due to oil (or discharged gas), which is introduced via the oil passage **125a** of the crankshaft **125**, may be formed inside the sealing member **144**.

An unexplained reference numeral **118** denotes a pressure separate plate, **118a** denotes a gas hole, and **118b** denotes an oil hole.

Hereinafter, description will be given of an operation effect of the scroll compressor with the aforementioned configuration.

That is, when power is applied to the driving motor **102**, the crankshaft **125** may rotate together with the rotor **122**, to transfer a rotational force to the orbiting scroll **104**.

The orbiting scroll **104** may accordingly orbit by an eccentric distance with respect to the main scroll **103**, thereby forming the first compression chamber S1 and the second compression chamber S2, which continuously move, between the fixed wrap **132** and the orbiting wrap **142**.

The first compression chamber S1 and the second compression chamber S2 may decrease in volume while moving toward the center by the continuously orbiting motion of the orbiting scroll **104**. Accordingly, a refrigerant introduced into each of the compression chambers S1 and S2 via the inlet **131b** may be compressed, and then discharged via the discharge port **131d** communicating with the inner final compression chamber.

The refrigerant discharged via the discharge port **131d** may flow into the inner space of the motor housing **111** via the discharge guide portion **174** of the bearing guide **107** and continuously flow into the pump housing **112** via the gas hole **118a** of the pressure separate plate **118**, thereby being introduced into a refrigerating cycle via the outlet **112c**.

Simultaneously, the oil pump **105** which is located at the rear end of the crankshaft **125** may operate to pump up oil stored in the pump housing **112**. The pumped oil may then be supplied into each bearing via the oil passage **125a**.

The oil may partially be collected back into the motor housing **111** via each bearing. Some of oil which is discharged together with the refrigerant discharged from the compression chambers may be separated from the refrigerant by the bearing guide **107** and then collected back into the motor housing **111**. The oil may then flow into the pump housing **112** via the oil hole **118b** of the pressure separate plate **118** due to pressure difference, be pumped by the oil pump **105**, and be supplied to each bearing, which series of operations may be repetitively executed.

As such, the main scroll forming the fixed scroll may be located between the motor housing and the front housing to be fixed to both of them. This may allow the fixed scroll to be installed without a separate frame, resulting in reduction of the number of components. In addition, the number of assembly parts may be reduced by coupling the motor housing, the main scroll and the front housing all together by use of long coupling bolts, reducing fabricating costs accordingly.

Also, the crankshaft may be inserted through the fixed wrap of the main scroll and the orbiting wrap of the orbiting scroll. This may allow an application point of a repulsive force of a refrigerant and an application point of a corresponding reaction point to be applied to the same portion, thereby preventing the orbiting scroll from being inclined. With forming the protrusion and the concave portion at the discharge side of the fixed wrap and the orbiting wrap, a compression ratio of a first compression chamber may be improved more than a scroll compressor having a fixed wrap and an orbiting wrap with an involute shape. Therefore, a thickness of an inner end portion of the fixed wrap may increase, which may result in improvement of a wrap strength and a leakage-preventing function.

11

Hereinafter, description will be given of the horizontal type scroll compressor having a plurality of pins as an anti-rotation member.

That is, the foregoing exemplary embodiment illustrates that the Oldham's ring having keys is applied as the anti-rotation member. However, for the Oldham's ring having the keys, keys and key recesses have to be formed on the Oldham's ring and the front housing and the orbiting scroll, which align with the Oldham's ring. This may cause difficulty in processing and increase fabricating costs. Further, a load of a motor may increase due to the heavy weight of the Oldham's ring and oil should be sufficiently supplied due to a wide frictional area of the Oldham's ring.

Considering such drawbacks, as shown in FIGS. 8 and 9, pin recesses 141e may be recessed into the front surface of the orbiting plate 141, and pin members 113d, which is orbitingly inserted into the pin recesses 141e to prevent rotation of the orbiting scroll 104, may be coupled to the front housing 113. The pin recesses 141e may be formed as many as the pin members 113d. Each of the pin recesses 141e may have an inner diameter enough for the pin member 113d to orbit smoothly therein. Accordingly, although the rotational force is transferred from the driving motor to the orbiting scroll, the pin members 113d may be inserted into the pin recesses 141e such that the pin recesses 141e can be restricted by the pin members 113d. This may allow the orbiting scroll to perform an orbiting motion without rotation.

Ring members 148 may be press-fitted to an inner circumferential surface of the pin recesses 141e, respectively, to prevent the abrasion of the pin recesses 141e due to friction against the pin members 113d. The ring member 148 may be made of a material whose strength is not smaller than that of the pin member 113d. The ring member 148 may also preferably be formed of a material having high abrasion resistance or a self-lubricating material to enhance a lubricative property with the pin member 113d without a separate oil supply.

Here, the pin recesses may be formed on the front housing and the pin members may be formed on the orbiting scroll. However, considering that the ring members be taken off while assembling the ring members to the pin recesses, the pin recesses may more preferably be formed on the front surface of the orbiting scroll. An unexplained reference numeral 113e denotes a groove forming a back pressure chamber.

As such the anti-rotation member implemented by the pin members and the pin recesses is disposed between the orbiting scroll and the front housing, the structure of the anti-rotation member may be simplified and the structures of the orbiting scroll and the front housing may also be simplified. This may facilitate for the fabrication of the orbiting scroll and the front housing as well as the anti-rotation member, resulting in reduction of fabricating costs of the orbiting scroll and the front housing contacting the anti-rotation member as well as the anti-rotation member.

Also, a load of a motor may be reduced by minimizing the weight of the anti-rotation member, and a frictional area may be minimized due to a linear contact between the pin member and the pin recess. Consequently, although a less amount of oil is supplied or oil is not temporarily supplied, the rotation of the orbiting scroll may effectively be prevented, enhancing design flexibility of the compressor.

In the meantime, the anti-rotation member may be implemented as an Oldham's ring (hereinafter, referred to as a ring member) which is made by removing keys from the general Oldham's ring.

12

For example, as shown in FIGS. 10 and 11, a first guide surface 141f and a second guide surface 113f may be orthogonally formed on the front surface of the orbiting scroll 104 and the rear surface of the front housing 113, respectively. A first sliding surface 165a and a second sliding surface 165b may be formed on the inner circumferential surface and the outer circumferential surface of the ring member 165, respectively, to be slidably contactable with the first guide surface 141f and a second guide surface 113f.

The first guide surface 141f and the second guide surface 113f may be provided in plurality, respectively, to be orthogonal to each other. The first sliding surface 165a and the second sliding surface 165d may be provided in plurality, respectively, to be orthogonal to each other.

Although the orbiting scroll 104 receives the rotational force from the driving motor 102, the first sliding surfaces 165a and the second sliding surfaces 165b of the ring member 165 and the first guide surfaces 141f and the second guide surfaces 113f may contact each other and be restricted by each other in a perpendicular direction. Therefore, the orbiting scroll 104 may perform the orbiting motion without rotation.

Even in this structure, the simplified structure of the anti-rotation member may facilitate for the fabrication thereof, which may result in reduction of fabricating costs of the orbiting scroll and the front housing contacting the anti-rotation member as well as the anti-rotation member. Also, a load of a motor may be reduced by virtue of reduction of the weight of the anti-rotation member.

The invention claimed is:

1. A horizontal type scroll compressor comprising:

a motor housing having an inner space for installation of a driving motor therein;

a main scroll coupled to one side of the motor housing to seal the inner space of the motor housing, and having a fixed wrap to form compression chambers;

an orbiting scroll having an orbiting wrap engaged with the fixed wrap of the main scroll and coupled to a crankshaft inserted through the main scroll, wherein the orbiting scroll forms a first compression chamber and a second compression chamber on an outer surface and an inner surface of the orbiting wrap while performing an orbiting motion; and

a front housing hermetically coupled to the main scroll, wherein the front housing accommodates the orbiting scroll, wherein a plurality of coupling bores is formed on the motor housing in a circumferential direction, and a plurality of through holes aligning with the plurality of coupling bores of the motor housing is formed through the main scroll and the front housing, respectively, and wherein the main scroll and the front housing are coupled to the motor housing using bolts inserted into the plurality of coupling bores through the plurality of through holes.

2. The compressor of claim 1, wherein an inlet is formed on an outer circumferential surface of the main scroll, and a discharge port is formed on one side surface of the main scroll facing the inner space of the motor housing.

3. The compressor of claim 2, wherein a bearing that supports the crankshaft is provided on one side surface of the main scroll, and wherein the bearing is installed on a bearing guide coupled to the main scroll.

4. The compressor of claim 1, wherein each of the motor housing, the main scroll, and the front housing is provided with at least one reference recess and at least one reference

13

hole in an aligning manner such that at least one reference pin is inserted into the at least one reference recess and the at least one reference hole.

5. A horizontal type scroll compressor comprising:

a casing having a motor housing and a front housing;

a driving motor installed within an inner space of the motor housing and having a rotor;

a crankshaft coupled to the rotor;

a main scroll having a fixed wrap, and provided between the motor housing and the front housing; and

an orbiting scroll having an orbiting wrap engaged with the fixed wrap of the main scroll and coupled to a crankshaft inserted through the main scroll, wherein the orbiting scroll forms a first compression chamber and a second compression chamber on an outer surface and an inner surface of the orbiting wrap while performing an orbiting motion, wherein a shaft coupling portion to which the crankshaft is inserted is formed through the orbiting scroll, wherein the orbiting scroll is accommodated within the front housing wherein a plurality of coupling bores is formed on the motor housing in a circumferential direction, and a plurality of through holes aligning with the plurality of coupling bores of the motor housing is formed through the main scroll and the front housing, respectively, and wherein the main scroll and the front housing are coupled to the motor housing using bolts inserted into the plurality of coupling bores through the plurality of through holes.

6. The compressor of claim 5, further including a bearing formed on an inner circumferential surface of the shaft coupling portion to support the crankshaft.

7. The compressor of claim 5, wherein an eccentric pin is formed on a front end of the crankshaft, and a bush is inserted into the eccentric pin so as to be inserted into the bearing provided on the shaft coupling portion, and wherein a snap ring that supports the bush in an axial direction is coupled to the eccentric pin.

8. The compressor of claim 5, wherein the casing includes a front housing hermetically coupled to the main scroll that accommodates the orbiting scroll therein, and wherein a sealing member is installed between the orbiting scroll and the front housing such that a back pressure chamber is formed around the shaft coupling portion that accommodates the shaft coupling portion therein.

9. The compressor of claim 8, wherein an oil passage is formed through the crankshaft in an axial direction, and the oil passage communicates with the back pressure chamber.

14

10. The compressor of claim 5, wherein the motor housing is hermetically coupled to one side surface of the main scroll, the motor housing having the driving motor installed therein, wherein a pump housing is coupled to another end of the motor housing to seal an inner space of the motor housing, wherein the pump housing accommodates an oil pump provided at an end portion of the crankshaft, and wherein a pressure separate plate having a gas hole and an oil hole is installed between the motor housing and the pump housing.

11. The compressor of claim 1, wherein a plurality of pin members is provided on one of a rear surface of the orbiting scroll or a casing, and a plurality of pin recesses is formed on the other one, and wherein the plurality of pin members is inserted into the plurality of pin recesses to allow for orbiting of the orbiting scroll.

12. The compressor of claim 11, wherein a ring member is inserted into each of the plurality of pin recesses, the ring member being formed of a material having a higher abrasion resistance than an abrasion resistance of the pin member.

13. The compressor of claim 1, wherein a ring member is provided between a rear surface of the orbiting scroll and a casing, the ring member preventing rotation of the orbiting scroll, and wherein an inner circumferential sliding surface and an outer circumferential sliding surface are perpendicularly formed on an inner circumferential surface and an outer circumferential surface of the ring member, respectively, the sliding surfaces slidably contacting guide surfaces, respectively, in a radial direction, the guide surfaces being provided on the casing and the orbiting scroll, respectively.

14. The compressor of claim 5, wherein the first compression chamber is formed between two contact points generated as an inner surface of the fixed wrap and an outer surface of the orbiting wrap contact each other, wherein the crankshaft includes an eccentric pin coupled to a shaft coupling portion of the orbiting scroll, and wherein $\alpha < 360^\circ$ at least before a beginning of discharging when α is a larger angle of angles formed by two lines connecting a center of the eccentric pin of the crankshaft and the two contact points, respectively.

15. The compressor of claim 5, wherein each of the motor housing, the main scroll, and the front housing is provided with at least one reference recess and at least one reference hole in an aligning manner such that the at least one reference pin is inserted into the at least one reference recess and the at least one reference hole.

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